

Controlling Seismic Effect on Bare RCC Frame by Lateral Force Resisting Systems (LFRS)

^[1] Durgesh Kumar Arya, ^[2] Anurag Bajpai, ^[3] Kumar Vanshaj

^[1] M.Tech Scholar (Structural Engineering), ^[2] Assistant Professor, ^[3] Ph.D. Scholar (Civil Engineering)

^{[1][2][3]} Department of Civil Engineering, Institute of Engineering & Technology, Lucknow, India

^{[1][2][3]} 1705205003@ietlucknow.ac.in

Abstract—In present scenario, the construction industry required high-rise and lighter structures, as tall and lighter structures are having more flexibility and small damping value so that it is less efficient to resist seismic responses. They are more susceptible to failure possibilities, LFRS to be provided to the tall structure which will result in reduction in the vibration induced by seismic and wind actions. Lateral Force Resisting System is big, heavy piece, which is constructed or installed from bottom to top of the tall structure and at different locations of the tall structure in plan and elevation. LFRS is either shear wall or bracing or combination of Shear Wall and Bracing. LFRS is installed in the tall RCC structures at various suitable locations. This research work concerned with controlling the tall RCC structural seismic effect by using lateral force resisting system (LFRS). LFRS are arranged in combinations and attached at different locations in the building. To study the seismic behaviour of tall lateral load resisting structure by taking either shear wall or bracing or combination of Shear Wall and Bracing using Response Spectrum Analysis method on ETABS v17.0.1 software. From this study the result obtained to find most effective arrangement on the basis of seismic parameters (time period, base shear distribution, max. storey displacement, storey drift & storey stiffness) and find out best suitable arrangement at given condition.

Keywords— Bracing, LFRS, Bare frame, Response Spectrum Analysis, Shear Wall etc

1. INTRODUCTION

In structural engineering, structural system is critical to good seismic performance of buildings. While moment-frame is the most commonly used lateral load resisting structural system, other structural systems also are commonly used like structural walls, frame-wall system, and braced-frame system. Lateral loads resulting from wind and seismic activities are now dominant in design considerations. Lateral displacement of such buildings must be strictly controlled, not only for occupants comfort and safety, but also to control secondary structural effects. Currently, there are many structural systems such as:

1. moment-frame
2. Structural walls
3. Frame-wall system and
4. Braced-frame system

The main objective of the study is investigate the seismic performance of a tall RCC frame building with X-Type bracing and shear wall by using Response Spectrum Analysis method and to study the seismic behaviour of tall lateral load resisting structure by taking combinations of shear wall & X-Type bracing using Response Spectrum Analysis method. Analysis is performed by Response Spectrum Analysis using ETABS 17.0.1 software.

2. BUILDING DESCRIPTION

Description of Residential building with 28 storeys Located in Delhi (NCR) are given below

A. Geometrical properties:

| S. No | Property Description | | Dimension |
|-------|----------------------------|---------------------|---------------|
| 1. | Floor height | | 3m |
| 2. | Height of building | | 84m |
| 3. | Area (plan) | | 31.5m x 31.5m |
| 4. | Beam dimension | | 300mm x 400mm |
| 5. | Columns (Inner and Corner) | Storey 1st to 14th | 500mm x 500mm |
| | Columns (Periphery) | | 300mm x 600mm |
| | Columns (Inner and Corner) | Storey 15th to 28th | 400mm x 400mm |
| | Columns (Periphery) | | 300mm x 500mm |
| 6. | Bracing | | ISLB 175 |
| 7. | No. of bays in X-direction | | 7No. @4.5m |
| 8. | No. of bays in Y-direction | | 7No. @4.5m |
| 9. | Slab thickness | | 150mm |
| 10. | Shear Wall thickness | | 200mm |

B. Material properties:

| S. No | Material | Grade |
|-------|--------------------------------------------|-------|
| 1. | Concrete (column, beam ,slab & shear wall) | M30 |
| 2. | Rebar | Fe500 |

C. Seismic data:

| | | |
|----|---------------------------|--------------------|
| 1. | Earthquake Zone – IV | Z = 0.24 |
| 2. | Damping | 5% |
| 3. | Importance Factor | 1.2 |
| 4. | Type of soil | Medium soil |
| 5. | Response Reduction Factor | 5 |
| 6. | Time Period | Program calculated |

D. Loading:

1. Live load 3.5kN/m² as per IS 875 part-II
2. Dead load as per IS 875 part-I
3. Earthquake load as per IS 1893:2016 part-I

3. PLAN AND 3D VIEW OF BUILDING FOR DIFFERENT MODELS

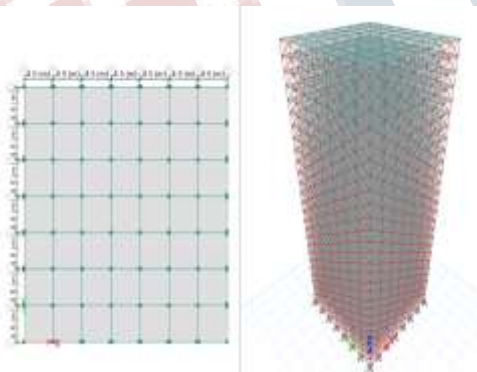


Figure1: Model 1 (X-Type bracing)

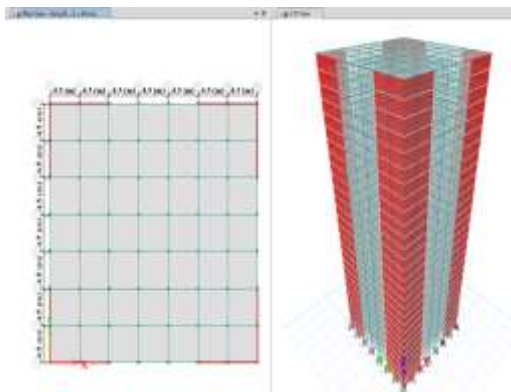


Figure2: Model 2 (Shear Wall at corner)

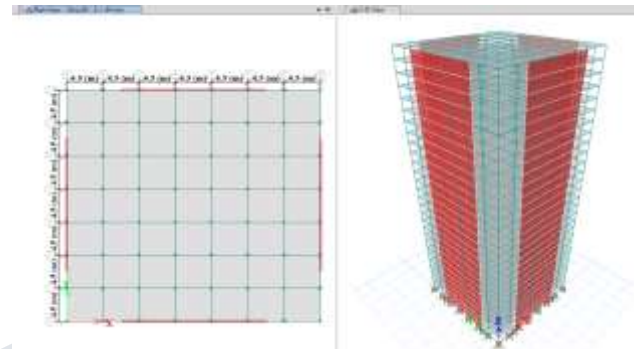


Figure3: Model 3 (Shear Wall at side center)

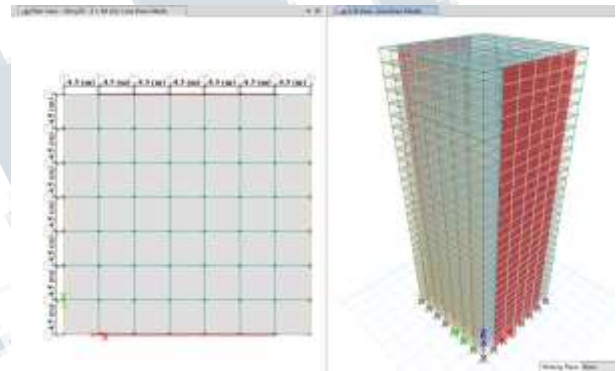


Figure4: Model 4 (Shear Wall on opposite face & X-Type bracing on opposite face)

4. METHOD OF ANALYSIS

A response spectrum is simply a plot of the peak response (displacement, velocity or acceleration) of a number of SDOF systems of varying natural period that are forced into motion by the same base vibration. The resulting plot can then be used to find the response of any structure, knowing its natural period. The plan shape used for analysis is “Square” shape tall building.

5. ANALYSIS RESULTS

The analysis of all the models that include RCC frame with X-Type bracing system, RCC frame with Shear Wall at different locations in plan and RCC frame with Shear Wall on opposite face & bracing on opposite face has been done and results are shown below. The parameters which were studied are on the behavior of building during seismic excitation are time period, base shear distribution, max. storey displacement, storey drift & storey stiffness.

(a) Natural Time Period

| Mode | MODE L 1 (sec) | MODE L 2 (sec) | MODE L 3 (sec) | MODE L 4 (sec) |
|------|----------------|----------------|----------------|----------------|
| 1 | 3.747 | 2.655 | 2.273 | 3.735 |
| 2 | 3.747 | 2.655 | 2.273 | 2.297 |
| 3 | 2.144 | 1.434 | 1.369 | 1.577 |
| 4 | 1.228 | 0.637 | 0.537 | 1.232 |
| 5 | 1.228 | 0.637 | 0.537 | 0.689 |
| 6 | 0.721 | 0.341 | 0.334 | 0.531 |
| 7 | 0.681 | 0.285 | 0.244 | 0.483 |
| 8 | 0.681 | 0.285 | 0.244 | 0.419 |
| 9 | 0.479 | 0.175 | 0.153 | 0.37 |
| 10 | 0.479 | 0.175 | 0.153 | 0.301 |
| 11 | 0.431 | 0.155 | 0.153 | 0.253 |
| 12 | 0.367 | 0.124 | 0.111 | 0.241 |

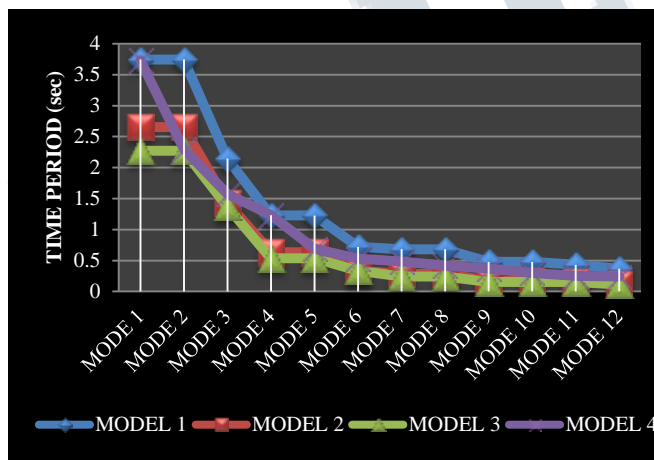


Figure5: Natural Time Period v/s Mode

All the objects of structure have a tendency to vibrate. The rate at which it wants to vibrate is its fundamental time period (natural time period) or un-damped free vibration of a structure. Structures that are weighty (with larger mass *m*) and flexibility (with smaller stiffness *k*) have greater natural time period than light and rigid structures.

The natural time period of vibration (*T*) in seconds are given below

$$T = 2\pi \sqrt{\frac{m}{k}}$$

Where,

K= Stiffness

M= Mass of Structure.

Model 1 shows maximum time period while model 3 shows minimum time period which means that model 1 is most flexible and model 3 is least flexible.

(b) Base Shear Distribution

| Storey | X-direction | | | |
|--------|--------------|--------------|--------------|--------------|
| | MODEL 1 (kN) | MODEL 2 (kN) | MODEL 3 (kN) | MODEL 4 (kN) |
| 1 | 0.7146 | 1.0804 | 1.2621 | 1.2071 |
| 2 | 2.8586 | 4.3216 | 5.0482 | 4.8285 |
| 3 | 6.4318 | 9.7236 | 11.3585 | 10.8642 |
| 4 | 11.4343 | 17.2864 | 20.1929 | 19.3141 |
| 5 | 17.8662 | 27.01 | 31.5514 | 30.1783 |
| 6 | 25.7273 | 38.8945 | 45.434 | 43.4568 |
| 7 | 35.0177 | 52.9397 | 61.8407 | 59.1495 |
| 8 | 45.7374 | 69.1457 | 80.7716 | 77.2565 |
| 9 | 57.8863 | 87.5125 | 102.2265 | 97.7778 |
| 10 | 71.4646 | 108.0402 | 126.2056 | 120.713 |
| 11 | 86.4722 | 130.7286 | 152.7087 | 146.063 |
| 12 | 102.9091 | 155.5779 | 181.736 | 173.827 |
| 13 | 120.7752 | 182.5879 | 213.2874 | 204.006 |
| 14 | 138.8576 | 210.044 | 245.3599 | 234.618 |
| 15 | 158.2682 | 239.518 | 279.7895 | 267.48 |
| 16 | 180.074 | 272.5183 | 318.3383 | 304.332 |
| 17 | 203.2867 | 307.6476 | 359.3741 | 343.563 |
| 18 | 227.9062 | 344.906 | 402.8969 | 385.171 |
| 19 | 253.9325 | 384.2934 | 448.9068 | 429.156 |
| 20 | 281.3656 | 425.8099 | 497.4036 | 475.519 |
| 21 | 310.2056 | 469.4554 | 548.3875 | 524.26 |
| 22 | 340.4524 | 515.2299 | 601.8584 | 575.378 |
| 23 | 372.106 | 563.1335 | 657.8163 | 628.874 |
| 24 | 405.1665 | 613.1662 | 716.2612 | 684.748 |
| 25 | 439.6338 | 665.3279 | 777.1932 | 742.999 |
| 26 | 475.5079 | 719.6187 | 840.6121 | 803.627 |
| 27 | 512.7889 | 776.0385 | 906.5181 | 866.634 |
| 28 | 539.5006 | 790.1314 | 922.9805 | 896.573 |

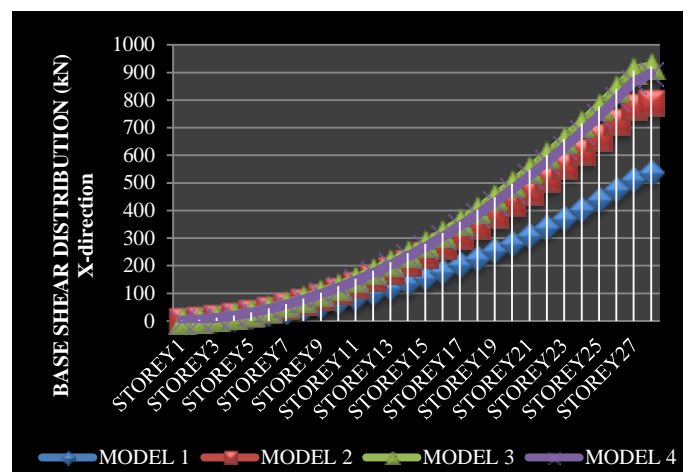


Figure6: Base Shear distribution in X-direction

Base shear is an approximation of the maximum lateral force that is occurs due to earthquake ground motion at the base of structure.

Model 1 shows minimum base shear while model 3 showing maximum base shear among these models for X-direction this means model 3 attract more shear force than model 1.

Base shear is an approximation of the maximum lateral force that is occurs due to earthquake ground motion at the base of structure.

Model 1 shows minimum base shear while model 3 showing maximum base shear among these models for Y-direction this means model 3 attract more shear force than model 1.

Y-direction

| Storey | Model 1 (kN) | Model 2 (kN) | Model 3 (kN) | Model 4 (kN) |
|--------|--------------|--------------|--------------|--------------|
| 1 | 0.7146 | 1.0804 | 1.2621 | 0.7426 |
| 2 | 2.8586 | 4.3216 | 5.0482 | 2.9705 |
| 3 | 6.4318 | 9.7236 | 11.3585 | 6.6835 |
| 4 | 11.4343 | 17.2864 | 20.1929 | 11.8818 |
| 5 | 17.8662 | 27.01 | 31.5514 | 18.5654 |
| 6 | 25.7273 | 38.8945 | 45.434 | 26.7341 |
| 7 | 35.0177 | 52.9397 | 61.8407 | 36.3881 |
| 8 | 45.7374 | 69.1457 | 80.7716 | 47.5274 |
| 9 | 57.8863 | 87.5125 | 102.2265 | 60.1518 |
| 10 | 71.4646 | 108.0402 | 126.2056 | 74.2615 |
| 11 | 86.4722 | 130.7286 | 152.7087 | 89.8564 |
| 12 | 102.9091 | 155.5779 | 181.736 | 106.9365 |
| 13 | 120.7752 | 182.5879 | 213.2874 | 125.5019 |
| 14 | 138.8576 | 210.044 | 245.3599 | 144.3343 |
| 15 | 158.2682 | 239.518 | 279.7895 | 164.5504 |
| 16 | 180.074 | 272.5183 | 318.3383 | 187.2218 |
| 17 | 203.2867 | 307.6476 | 359.3741 | 211.3559 |
| 18 | 227.9062 | 344.906 | 402.8969 | 236.9526 |
| 19 | 253.9325 | 384.2934 | 448.9068 | 264.012 |
| 20 | 281.3656 | 425.8099 | 497.4036 | 292.5341 |
| 21 | 310.2056 | 469.4554 | 548.3875 | 322.5188 |
| 22 | 340.4524 | 515.2299 | 601.8584 | 353.9662 |
| 23 | 372.106 | 563.1335 | 657.8163 | 386.8763 |
| 24 | 405.1665 | 613.1662 | 716.2612 | 421.249 |
| 25 | 439.6338 | 665.3279 | 777.1932 | 457.0845 |
| 26 | 475.5079 | 719.6187 | 840.6121 | 494.3826 |
| 27 | 512.7889 | 776.0385 | 906.5181 | 533.1433 |
| 28 | 539.5006 | 790.1314 | 922.9805 | 551.5617 |

(c) Max. Storey Displacement X-direction

| Storey | MODEL 1 (mm) | MODEL 2 (mm) | MODEL 3 (mm) | MODEL 4 (mm) |
|--------|--------------|--------------|--------------|--------------|
| 1 | 2.875 | 0.599 | 0.597 | 0.602 |
| 2 | 6.87 | 1.702 | 1.59 | 1.605 |
| 3 | 11.038 | 3.23 | 2.921 | 2.952 |
| 4 | 15.357 | 5.147 | 4.568 | 4.621 |
| 5 | 19.81 | 7.414 | 6.504 | 6.586 |
| 6 | 24.381 | 9.999 | 8.706 | 8.824 |
| 7 | 29.053 | 12.869 | 11.152 | 11.311 |
| 8 | 33.809 | 15.996 | 13.818 | 14.025 |
| 9 | 38.632 | 19.352 | 16.684 | 16.945 |
| 10 | 43.505 | 22.911 | 19.729 | 20.05 |
| 11 | 48.409 | 26.648 | 22.933 | 23.32 |
| 12 | 53.325 | 30.54 | 26.276 | 26.736 |
| 13 | 58.234 | 34.565 | 29.741 | 30.279 |
| 14 | 63.059 | 38.695 | 33.302 | 33.925 |
| 15 | 68.2 | 42.948 | 36.976 | 37.687 |
| 16 | 73.233 | 47.27 | 40.717 | 41.522 |
| 17 | 78.184 | 51.646 | 44.513 | 45.417 |
| 18 | 83.024 | 56.055 | 48.347 | 49.355 |
| 19 | 87.726 | 60.479 | 52.204 | 53.32 |
| 20 | 92.261 | 64.901 | 56.069 | 57.299 |
| 21 | 96.604 | 69.306 | 59.929 | 61.277 |
| 22 | 100.725 | 73.681 | 63.774 | 65.243 |
| 23 | 104.597 | 78.015 | 67.591 | 69.185 |
| 24 | 108.194 | 82.299 | 71.374 | 73.095 |
| 25 | 111.487 | 86.529 | 75.115 | 76.966 |
| 26 | 114.45 | 90.7 | 78.809 | 80.792 |
| 27 | 117.057 | 94.815 | 82.456 | 84.572 |
| 28 | 119.283 | 98.865 | 86.039 | 88.293 |

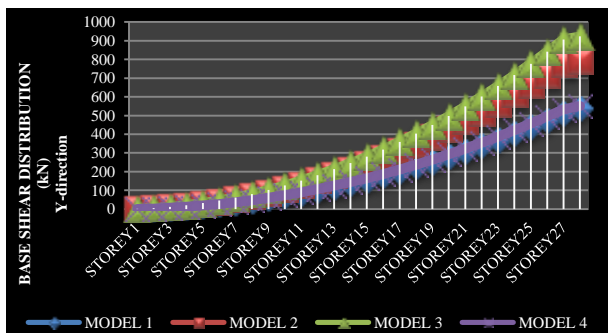


Figure7: Base Shear Distribution in Y-direction

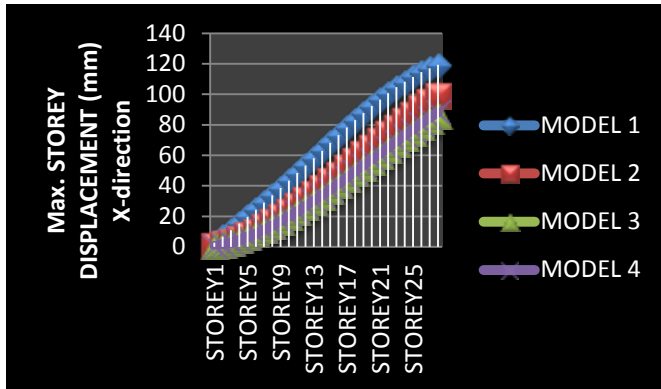


Figure8: Maximum storey displacement in X-direction

The Maximum storey displacement (X-direction) observed in model 1, model 2, model 3 & model 4 is respectively 119.283mm, 98.865mm, 86.039mm, 88.293mm which is under permissible limit of **IS1893:2016 code** i.e. 0.004 times of structure height (i.e. 336mm).

The percentage of reduction in max. storey displacement of model 2, model 3 & model 4 is respectively 17.11%, 27.86% & 25.98%.

Y-direction

| Storey | MODEL 1 (mm) | MODEL 2 (mm) | MODEL 3 (mm) | MODEL 4 (mm) |
|--------|--------------|--------------|--------------|--------------|
| 1 | 2.875 | 0.599 | 0.597 | 2.686 |
| 2 | 6.87 | 1.702 | 1.59 | 6.528 |
| 3 | 11.038 | 3.23 | 2.921 | 10.567 |
| 4 | 15.357 | 5.147 | 4.568 | 14.768 |
| 5 | 19.81 | 7.414 | 6.504 | 19.111 |
| 6 | 24.381 | 9.999 | 8.706 | 23.577 |
| 7 | 29.053 | 12.869 | 11.152 | 28.149 |
| 8 | 33.809 | 15.996 | 13.818 | 32.807 |
| 9 | 38.632 | 19.352 | 16.684 | 37.533 |
| 10 | 43.505 | 22.911 | 19.729 | 42.308 |
| 11 | 48.409 | 26.648 | 22.933 | 47.113 |
| 12 | 53.325 | 30.54 | 26.276 | 51.929 |
| 13 | 58.234 | 34.565 | 29.741 | 56.733 |
| 14 | 63.059 | 38.695 | 33.302 | 61.455 |
| 15 | 68.2 | 42.948 | 36.976 | 66.511 |
| 16 | 73.233 | 47.27 | 40.717 | 71.461 |
| 17 | 78.184 | 51.646 | 44.513 | 76.322 |
| 18 | 83.024 | 56.055 | 48.347 | 81.065 |
| 19 | 87.726 | 60.479 | 52.204 | 85.665 |
| 20 | 92.261 | 64.901 | 56.069 | 90.093 |
| 21 | 96.604 | 69.306 | 59.929 | 94.322 |
| 22 | 100.725 | 73.681 | 63.774 | 98.325 |
| 23 | 104.597 | 78.015 | 67.591 | 102.077 |

| | | | | |
|----|---------|--------|--------|---------|
| 24 | 108.194 | 82.299 | 71.374 | 105.552 |
| 25 | 111.487 | 86.529 | 75.115 | 108.724 |
| 26 | 114.45 | 90.7 | 78.809 | 111.57 |
| 27 | 117.057 | 94.815 | 82.456 | 114.067 |
| 28 | 119.283 | 98.865 | 86.039 | 116.16 |

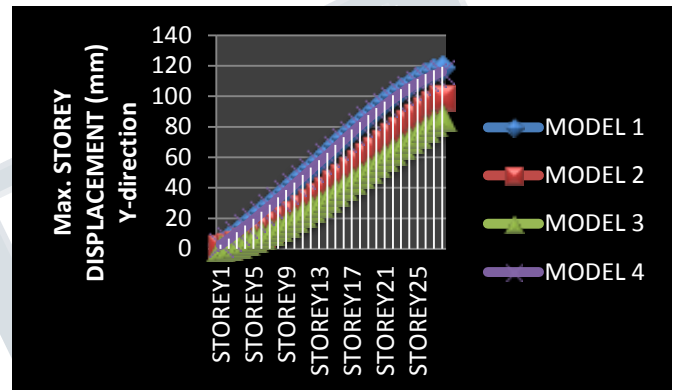


Figure9: Maximum storey displacement in Y-direction

The Maximum storey displacement (Y-direction) observed in model 1, model 2, model 3 & model 4 is respectively 119.283mm, 98.865mm, 86.039mm & 116.16mm which is under permissible limit of **IS1893:2016 code** i.e. 0.004 times of structure height (i.e. 336mm).

The percentage of reduction in max. storey displacement of model 2, model 3 & model 4 is respectively 17.11%, 27.86% & 2.61%.

(d) Storey Drift

X-direction

| Storey | MODEL 1 (mm) | MODEL 2 (mm) | MODEL 3 (mm) | MODEL 4 (mm) |
|--------|--------------|--------------|--------------|--------------|
| 1 | 2.875 | 0.599 | 0.597 | 0.602 |
| 2 | 3.995 | 1.102 | 0.994 | 1.003 |
| 3 | 4.168 | 1.528 | 1.33 | 1.347 |
| 4 | 4.319 | 1.917 | 1.647 | 1.669 |
| 5 | 4.453 | 2.268 | 1.936 | 1.965 |
| 6 | 4.571 | 2.585 | 2.202 | 2.238 |
| 7 | 4.672 | 2.87 | 2.445 | 2.487 |
| 8 | 4.756 | 3.127 | 2.666 | 2.714 |
| 9 | 4.823 | 3.356 | 2.866 | 2.92 |
| 10 | 4.873 | 3.559 | 3.045 | 3.105 |
| 11 | 4.904 | 3.737 | 3.204 | 3.27 |
| 12 | 4.916 | 3.892 | 3.343 | 3.415 |
| 13 | 4.909 | 4.025 | 3.465 | 3.543 |
| 14 | 4.825 | 4.13 | 3.562 | 3.646 |
| 15 | 5.142 | 4.253 | 3.674 | 3.762 |
| 16 | 5.033 | 4.322 | 3.741 | 3.835 |

| | | | | |
|----|-------|-------|-------|-------|
| 17 | 4.951 | 4.376 | 3.796 | 3.895 |
| 18 | 4.84 | 4.409 | 3.834 | 3.938 |
| 19 | 4.702 | 4.424 | 3.857 | 3.966 |
| 20 | 4.536 | 4.422 | 3.865 | 3.979 |
| 21 | 4.342 | 4.405 | 3.861 | 3.978 |
| 22 | 4.121 | 4.375 | 3.844 | 3.966 |
| 23 | 3.872 | 4.334 | 3.818 | 3.942 |
| 24 | 3.596 | 4.284 | 3.783 | 3.91 |
| 25 | 3.293 | 4.229 | 3.741 | 3.871 |
| 26 | 2.963 | 4.171 | 3.694 | 3.826 |
| 27 | 2.607 | 4.116 | 3.647 | 3.78 |
| 28 | 2.226 | 4.05 | 3.584 | 3.721 |

| | | | | |
|----|-------|-------|-------|-------|
| 11 | 4.904 | 3.737 | 3.204 | 4.805 |
| 12 | 4.916 | 3.892 | 3.343 | 4.816 |
| 13 | 4.909 | 4.025 | 3.465 | 4.804 |
| 14 | 4.825 | 4.13 | 3.562 | 4.722 |
| 15 | 5.142 | 4.253 | 3.674 | 5.056 |
| 16 | 5.033 | 4.322 | 3.741 | 4.951 |
| 17 | 4.951 | 4.376 | 3.796 | 4.86 |
| 18 | 4.84 | 4.409 | 3.834 | 4.744 |
| 19 | 4.702 | 4.424 | 3.857 | 4.599 |
| 20 | 4.536 | 4.422 | 3.865 | 4.428 |
| 21 | 4.342 | 4.405 | 3.861 | 4.229 |
| 22 | 4.121 | 4.375 | 3.844 | 4.004 |
| 23 | 3.872 | 4.334 | 3.818 | 3.752 |
| 24 | 3.596 | 4.284 | 3.783 | 3.474 |
| 25 | 3.293 | 4.229 | 3.741 | 3.172 |
| 26 | 2.963 | 4.171 | 3.694 | 2.846 |
| 27 | 2.607 | 4.116 | 3.647 | 2.497 |
| 28 | 2.226 | 4.05 | 3.584 | 2.093 |

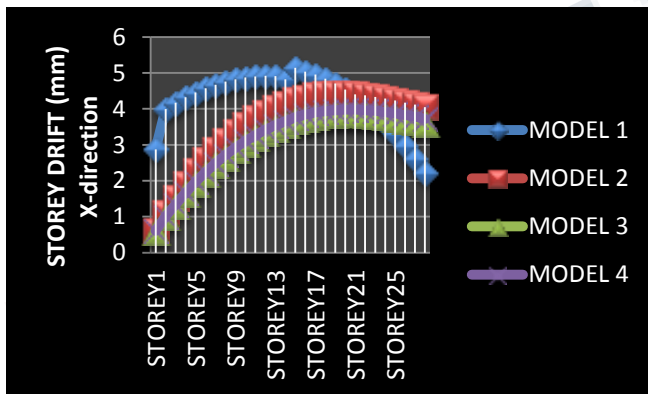


Figure10: Comparison of storey drift in X-direction

The storey drift in X-direction observed at 15th storey in model 1, model 2, model 3 & model 4 is respectively 5.142mm, 4.253mm, 3.674mm & 3.762mm which is under permissible limit of **IS 1893:2016** recommended value 0.004 times of storey height (i.e. 12 mm).

The percentage of reduction in storey drift of model 2, model 3 & model 4 is respectively 17.28% , 28.54% & 26.83%.

Y-direction

| Storey | MODEL 1 (mm) | MODEL 2 (mm) | MODEL 3 (mm) | MODEL 4 (mm) |
|--------|--------------|--------------|--------------|--------------|
| 1 | 2.875 | 0.599 | 0.597 | 2.686 |
| 2 | 3.995 | 1.102 | 0.994 | 3.841 |
| 3 | 4.168 | 1.528 | 1.33 | 4.04 |
| 4 | 4.319 | 1.917 | 1.647 | 4.201 |
| 5 | 4.453 | 2.268 | 1.936 | 4.343 |
| 6 | 4.571 | 2.585 | 2.202 | 4.466 |
| 7 | 4.672 | 2.87 | 2.445 | 4.571 |
| 8 | 4.756 | 3.127 | 2.666 | 4.658 |
| 9 | 4.823 | 3.356 | 2.866 | 4.726 |
| 10 | 4.873 | 3.559 | 3.045 | 4.775 |

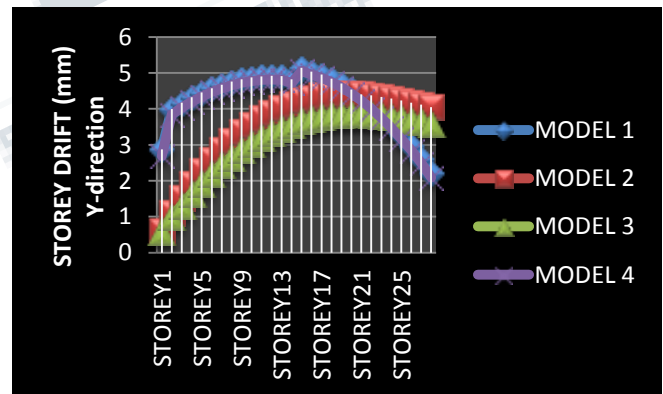


Figure11: Comparison of storey drift in Y-direction

The storey drift in Y-direction observed at 15th storey in model 1, model 2, model 3 & model 4 is respectively 5.142mm, 4.253mm, 3.674mm & 5.056mm which is under permissible limit of **IS 1893:2016** recommended value 0.004 times of storey height (i.e. 12 mm).

The percentage of reduction in storey drift of model 2, model 3 & model 4 is respectively 17.28% , 28.54% & 1.67%.

(e) Storey Stiffness

X-direction

| Storey | MODEL 1 (kN/m) | MODEL 2 (kN/m) | MODEL 3 (kN/m) | MODEL 4 (kN/m) |
|--------|----------------|----------------|----------------|----------------|
| 1 | 3111734 | 2581049 | 2974564 | 2947907 |
| 2 | 2243394 | 1553866 | 2007137 | 1983114 |

| | | | | |
|----|----------|--------------|--------------|--------------|
| | | 8 | 6 | 8 |
| 3 | 2162830 | 1167782 8 | 1578086 8 | 1554263 7 |
| 4 | 2092963 | 9428489 | 1298208 5 | 1276455 8 |
| 5 | 2027697 | 7937265 | 1103079 9 | 1082184 8 |
| 6 | 1967378 | 6845548 | 9552438 | 9338440 |
| 7 | 1912192 | 5999640 | 8377187 | 8150458 |
| 8 | 1861434 | 5318193 | 7407018 | 7168664 |
| 9 | 1814174 | 4753866 | 6587269 | 6344517 |
| 10 | 1769969 | 4277186 | 5888276 | 5649207 |
| 11 | 1728860 | 3870871 | 5295212 | 5064325 |
| 12 | 1690736 | 3526939 | 4799894 | 4576769 |
| 13 | 1655105 | 3242676 | 4394529 | 4175453 |
| 14 | 1639634 | 3024769 | 4082284 | 3860779 |
| 15 | 1488752 | 2837642 | 3812513 | 3590079 |
| 16 | 1468865 | 2723941 | 3645666 | 3413820 |
| 17 | 1435579 | 2644158 | 3532388 | 3292103 |
| 18 | 1405574 | 2589631 | 3463297 | 3219478 |
| 19 | 1377772 | 2549463 | 3418066 | 3179950 |
| 20 | 1350867 | 2515304 | 3376024 | 3153699 |
| 21 | 1324104 | 2478895 | 3318828 | 3118136 |
| 22 | 1297312 | 2428879 | 3230560 | 3049752 |
| 23 | 1268910 | 2348689 | 3094880 | 2925589 |
| 24 | 1232691 | 2216511 | 2891445 | 2724126 |
| 25 | 1175237 | 2007216 | 2594413 | 2425739 |
| 26 | 1073740 | 1695487 | 2174861 | 2013269 |
| 27 | 891082.5 | 1258572 | 1604152 | 1471639 |
| 28 | 563129.3 | 684474.9 | 868485.2 | 793811.6 |

Y-direction

| Storey | MODEL 1 (kN/m) | MODEL 2 (kN/m) | MODEL 3 (kN/m) | MODEL 4 (kN/m) |
|--------|----------------|----------------|----------------|----------------|
| 1 | 3111734 | 2581049 3 | 2974564 3 | 3234613 |
| 2 | 2243394 | 1553866 8 | 2007137 6 | 2287183 |
| 3 | 2162830 | 1167782 8 | 1578086 8 | 2200559 |
| 4 | 2092963 | 9428489 | 1298208 5 | 2131738 |
| 5 | 2027697 | 7937265 | 1103079 9 | 2069369 |
| 6 | 1967378 | 6845548 | 9552438 | 2012565 |
| 7 | 1912192 | 5999640 | 8377187 | 1960634 |
| 8 | 1861434 | 5318193 | 7407018 | 1913455 |
| 9 | 1814174 | 4753866 | 6587269 | 1870850 |
| 10 | 1769969 | 4277186 | 5888276 | 1831708 |
| 11 | 1728860 | 3870871 | 5295212 | 1794788 |
| 12 | 1690736 | 3526939 | 4799894 | 1759781 |
| 13 | 1655105 | 3242676 | 4394529 | 1727873 |
| 14 | 1639634 | 3024769 | 4082284 | 1716887 |
| 15 | 1488752 | 2837642 | 3812513 | 1554527 |
| 16 | 1468865 | 2723941 | 3645666 | 1538028 |
| 17 | 1435579 | 2644158 | 3532388 | 1509858 |
| 18 | 1405574 | 2589631 | 3463297 | 1482554 |
| 19 | 1377772 | 2549463 | 3418066 | 1456089 |
| 20 | 1350867 | 2515304 | 3376024 | 1430685 |
| 21 | 1324104 | 2478895 | 3318828 | 1407289 |
| 22 | 1297312 | 2428879 | 3230560 | 1384315 |
| 23 | 1268910 | 2348689 | 3094880 | 1357680 |
| 24 | 1232691 | 2216511 | 2891445 | 1323203 |
| 25 | 1175237 | 2007216 | 2594413 | 1273902 |
| 26 | 1073740 | 1695487 | 2174861 | 1189243 |
| 27 | 891082.5 | 1258572 | 1604152 | 1021465 |
| 28 | 563129.3 | 684474.9 | 868485.2 | 683284.5 |

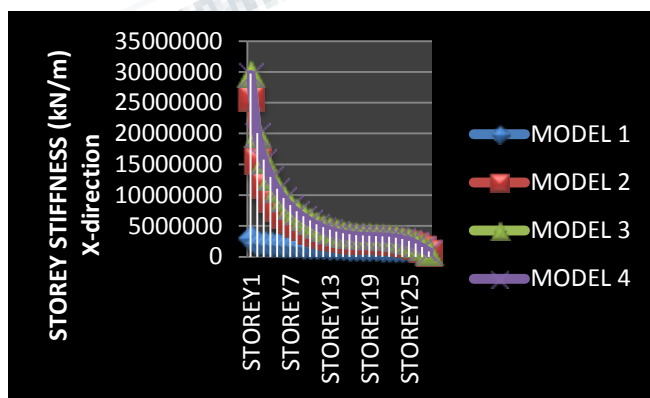


Figure12: Comparison of storey stiffness in X-direction

The maximum value of stiffness (X-direction) observed in model 3, so model 3 gives better response among all models. The storey stiffness of model 2 is 8.29 times, model 3 is 9.55 times & model 4 is 9.47 times more than the model 1.

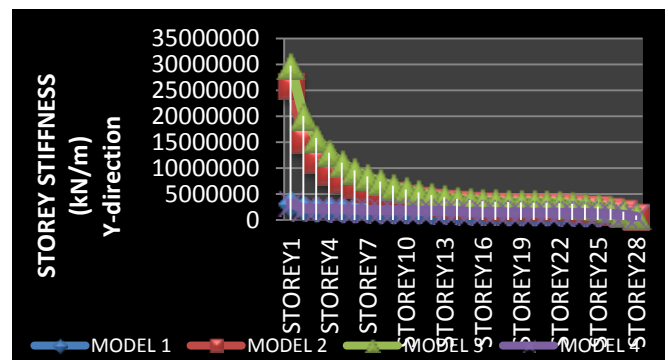


Figure13: Comparison of storey stiffness in Y-direction

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The maximum value of stiffness (Y-direction) observed in model 3, so model 3 gives better response among all models. The storey stiffness of model 2 is 8.29 times, model 3 is 9.55 times & model 4 is 1.03 times more than the model 1.

6. CONCLUSION

In this paper the buildings with LFRS are studied and the seismic parameters in terms of Time period, Base shear distribution, Maximum storey displacement, Storey drift and storey stiffness are compared. The following conclusions are summarized based on analysis:

1. In this research work model 1 shows maximum time period while model 3 shows minimum time period which means that model 1 is most flexible and model 3 is least flexible.
2. The maximum displacement of the building was found to be minimum in shear wall at side center while Model 1 shows maximum displacement. and is at verge of failure as per standards. Model 1 showed higher storey displacement that it is more prone to damage during earthquake as compared to other models with LFRS.
3. Model 1 is show maximum drift while other models are shows less drift. All models with LFRS satisfying criteria maximum allowed storey drift as per Indian standards i.e. 0.004 times of storey height.
4. In tall buildings, the storey stiffness is one of the important factor. So for this lateral force resisting systems are adopted to enhance this parameter. Model 3(shear wall at side center) showing maximum stiffness while Model 1(X-type bracing) has minimum stiffness.
5. It can also be observed that as we move upward the storey stiffness decreased in all four models so no soft storey effect is observed in any model.
6. A sudden change in the stiffness has been observed at 15th storey due to change in column size at 15 storey.

From the above discuss it can be concluded that shear wall at side center shows best result when compared with X-type bracing, shear wall at corner and and RCC frame with Shear Wall on opposite face & bracing on opposite face.

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